



AP61204Q

## AUTOMOTIVE-COMPLIANT, 5.5V INPUT, 2A LOW IQ SYNCHRONOUS BUCK CONVERTER

# **Description**

The AP61204Q is an automotive-compliant, 2A, synchronous buck converter with a wide input-voltage range of 2.4V to 5.5V. The device fully integrates a  $70m\Omega$  high-side power MOSFET and a  $50m\Omega$  low-side power MOSFET to provide high-efficiency step-down DC-DC conversion.

The AP61204Q device is easily used by minimizing the external component count due to its adoption of Constant On-Time (COT) control to achieve fast transient response, easy loop stabilization, and low output-voltage ripple.

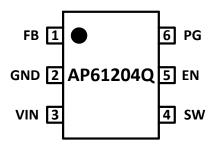
The device is available in a SOT563 package.

## **Features**

- AEC-Q100 Qualified for Automotive Applications
  - Device Temperature Grade 1: -40°C to +125°C T<sub>A</sub> Range
- VIN: 2.4V to 5.5V
- Output Voltage (VOUT): 0.6V to VIN
- 2A Continuous Output Current
- 0.6V ± 2% Reference Voltage
- 19µA Low Quiescent Current (Pulse-Frequency Modulation)
- 2.4MHz Switching Frequency (VIN = 5V, VOUT = 1.8V)
- Up to 84% Efficiency at 5mA Light Load
- Programmable Operation Mode Through EN
  - Pulse-Frequency Modulation
  - Pulse-Width Modulation Regardless of Output Load
- Low-Dropout (LDO) Mode
- Power-Good Indicator
- Protection Circuitry
  - Undervoltage Lockout (UVLO)
  - VIN Overvoltage Protection (OVP)
  - Peak Current Limit
  - Valley Current Limit
  - Thermal Shutdown
- Totally Lead-Free & Fully RoHS Compliant (Notes 1 & 2)
- Halogen and Antimony Free. "Green" Device (Note 3)
- The AP61204Q is suitable for automotive applications requiring specific change control; this part is AEC-Q100 qualified, PPAP capable, and manufactured in IATF 16949 certified facilities.

https://www.diodes.com/quality/product-definitions/

## **Pin Assignments**



**SOT563** 

## **Applications**

- Automotive power systems
- Automotive infotainment
- Automotive instrument clusters
- Automotive telematics
- Advanced driver assistance systems

Notes:

- 1. No purposely added lead. Fully EU Directive 2002/95/EC (RoHS), 2011/65/EU (RoHS 2) & 2015/863/EU (RoHS 3) compliant.
- 2. See https://www.diodes.com/quality/lead-free/ for more information about Diodes Incorporated's definitions of Halogen- and Antimony-free, "Green" and Lead-free.
- 3. Halogen- and Antimony-free "Green" products are defined as those which contain <900ppm bromine, <900ppm chlorine (<1500ppm total Br + Cl) and <1000ppm antimony compounds.



# **Typical Application Circuit**

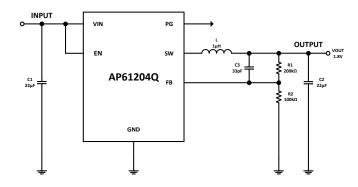


Figure 1. Typical AP61204Q Application Circuit

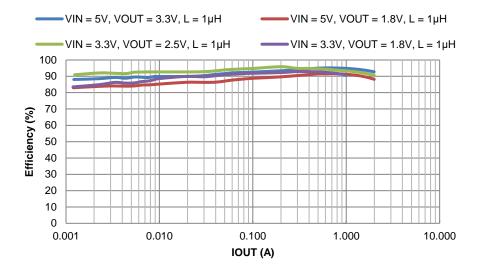


Figure 2. PFM Efficiency vs. Output Current

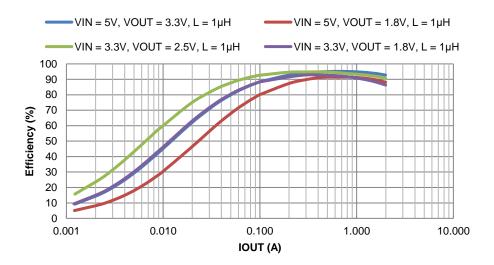


Figure 3. PWM Efficiency vs. Output Current



# **Pin Descriptions**

Pin Name	Pin Number	Function
FB	1	Feedback sensing terminal for the output voltage. Connect this pin to the resistive divider of the output. See Setting the Output Voltage section for more details.
GND	2	Power Ground.
VIN	3	Power Input. VIN supplies the power to the IC as well as the step-down converter power MOSFETs. Drive VIN with a 2.4V to 5.5V power source. Bypass VIN to GND with a suitably large capacitor to eliminate noise due to the switching of the IC. See <i>Input Capacitor</i> section for more details.
SW	4	Power Switching Output. SW is the switching node that supplies power to the output. Connect the output LC filter from SW to the output load.
EN	5	Enable Input. EN is a digital input that turns the regulator on or off. Drive EN high to turn on the regulator and low to turn it off. EN is used to program the Operation Mode (PFM or PWM). See <i>Enable</i> section for more details.
PG	6	Power-Good. Open-drain power-good output that is pulled to GND when the output voltage is out of its regulation limits or during soft-start.

# **Functional Block Diagram**

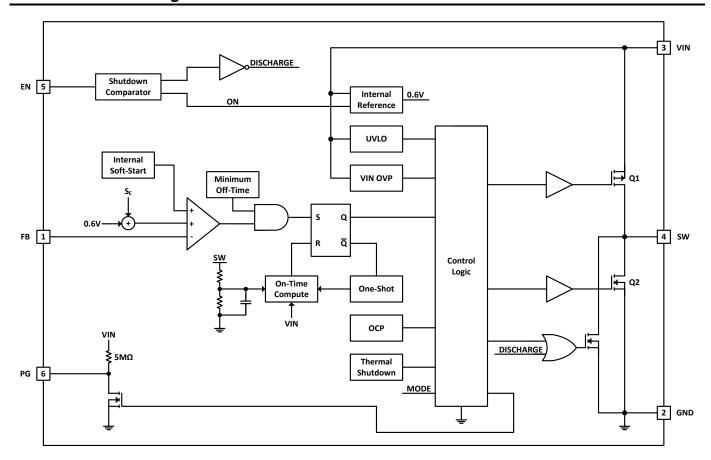


Figure 4. Functional Block Diagram



## Absolute Maximum Ratings (Note 4) (@ TA = +25°C, unless otherwise specified.)

Symbol	Parameter	Rating	Unit
VIN	Cupply Dip Voltage	-0.3 to +6.5 (DC)	V
VIIN	Supply Pin Voltage	-0.3 to +7.0 (400ms)	V
VFB	Feedback Pin Voltage	-0.3 to VIN + 0.3	V
	Cuitab Din Valtage	-1.0 to VIN + 0.3 (DC)	V
V <sub>SW</sub>	Switch Pin Voltage	-2.5 to VIN + 2.0 (20ns)	V
Ven	Enable Pin Voltage	-0.3 to VIN + 0.3	V
Vpg	Power-Good Pin Voltage	-0.3 to +6.0 (DC)	V
T <sub>ST</sub>	Storage Temperature	-65 to +150	°C
TJ	Junction Temperature	+160	°C
TL	Lead Temperature	+260	°C
ESD Susceptibility	(Note 5)		
НВМ	Human Body Model	±4000	V
CDM	Charged Device Model	±1500	V

Notes:

## Thermal Resistance (Note 6)

Symbol	Parameter	JEDEC (Note 6)	EVM (Note 7)	Unit
θЈА	Junction to Ambient	141	60	°C/W
θ <sub>JC</sub>	Junction to Case	33	33	°C/W

Notes:

# Recommended Operating Conditions (Note 8) (@ TA = +25°C, unless otherwise specified.)

Symbol	Parameter	Min	Max	Unit
VIN	Supply Voltage	2.4	5.5	V
VOUT	Output Voltage	0.6	VIN	V
TJ	Operating Junction Temperature	-40	+150	°C

Note: 8. The device function is not guaranteed outside of the recommended operating conditions.

<sup>4.</sup> Stresses greater than those listed under *Absolute Maximum Ratings* can cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions* is not implied. Exposure to *Absolute Maximum Ratings* for extended periods can affect device reliability.

<sup>5.</sup> Semiconductor devices are ESD sensitive and can be damaged by exposure to ESD events. Suitable ESD precautions should be taken when handling and transporting these devices.

<sup>6.</sup> Test condition for SOT563: device mounted on FR-4 substrate, two-layer PCB, 2oz copper, with minimum recommended pad layout.

<sup>7.</sup> Device mounted on Diodes Incorporated's evaluation board.

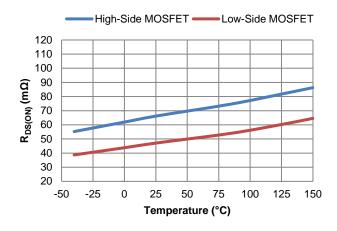


Symbol	Parameter	Conditions	Min	Тур	Max	Unit
Ishdn	Shutdown Supply Current	VEN = 0V	_	0.1	_	μA
1-	Quiescent Supply Current	PFM, V <sub>FB</sub> = 0.65V	_	19	_	μA
ΙQ	Quiescent Supply Current	PWM, V <sub>FB</sub> = 0.65V		690	_	μΑ
POR	VIN Power-on Reset Rising Threshold	_		2.3	2.4	٧
UVLO	VIN Undervoltage Lockout Falling Threshold	_	_	2.2	_	٧
OVPvin	VIN Overvoltage Rising Threshold	_	_	6.3	_	V
OVP <sub>VIN_HYS</sub>	VIN Overvoltage Hysteresis	_	_	300	_	mV
RDS(ON)1	High-Side Power MOSFET On-Resistance (Note 9)	_	_	70	_	mΩ
RDS(ON)2	Low-Side Power MOSFET On-Resistance (Note 9)	_	_	50	_	mΩ
IPEAK_LIMIT	HS Peak Current Limit (Note 9)	From Source to Drain	2.4	3.0	3.6	Α
IVALLEY_LIMIT	LS Valley Current Limit (Note 9)	From Source to Drain	_	2.6	_	Α
fsw	Oscillator Frequency	VOUT = 1.8V, CCM	1.9	2.4	2.9	MHz
ton_min	Minimum On-Time	_	_	70	_	ns
toff_min	Minimum Off-Time	_		70	_	ns
V <sub>FB</sub>	Feedback Voltage	ССМ	0.588	0.600	0.612	٧
Ven_h	EN Logic-High Threshold	_	_	0.91	_	V
V <sub>EN_L</sub>	EN Logic-Low Threshold	_		0.83	_	V
tss	Soft-Start Time	_	_	0.5	_	ms
PG <sub>UV_FALL</sub>	Undervoltage Falling Threshold	Percent of Output Regulation, Fault	_	90	_	%
PG <sub>UV_RISE</sub>	Undervoltage Rising Threshold	Percent of Output Regulation, Good	_	95	_	%
PGov_rise	Overvoltage Rising Threshold	Percent of Output Regulation, Fault	_	110	_	%
PGov_fall	Overvoltage Falling Threshold	Percent of Output Regulation, Good	_	105	_	%
tpg_rd	Power-Good Falling Delay Time	_	_	40	_	μs
Vpg_ol	Power-Good Output Logic Low	IPG = -1mA	_	_	0.4	V
R <sub>PG</sub>	Power-Good Pullup Resistor	_	_	5	_	МΩ
T <sub>SD</sub>	Thermal Shutdown (Note 9)	_	_	+160	_	°C
T <sub>Hys</sub>	Thermal Shutdown Hysteresis (Note 9)		_	+30	_	°C

Note: 9. Compliance to the datasheet limits is assured by one or more methods: production test, characterization, and/or design.



**Typical Performance Characteristics** (AP61204Q @ T<sub>A</sub> = +25°C, VIN = 5V, VOUT = 1.8V, BOM = Table 1, unless otherwise specified.)



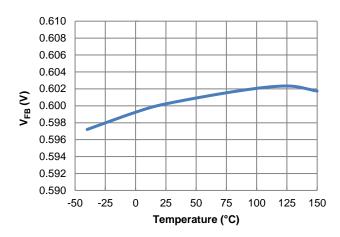
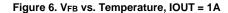
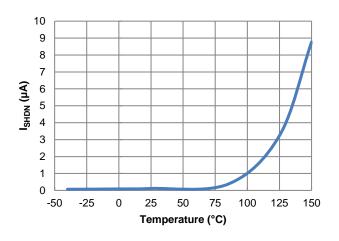


Figure 5. Power MOSFET RDS(ON) vs. Temperature





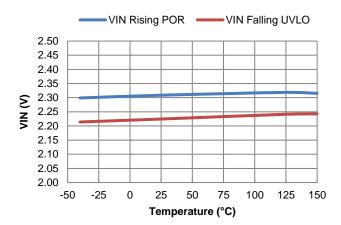


Figure 7. I<sub>SHDN</sub> vs. Temperature

Figure 8. VIN Power-On Reset and UVLO vs. Temperature



**Typical Performance Characteristics** (AP61204Q @ T<sub>A</sub> = +25°C, VIN = 5V, VOUT = 1.8V, BOM = Table 1, PFM, unless otherwise specified.)

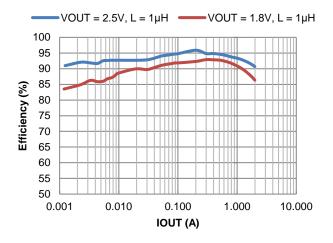


Figure 9. Efficiency vs. Output Current, VIN = 3.3V

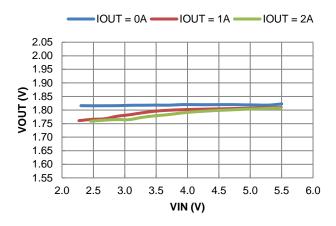


Figure 11. Line Regulation

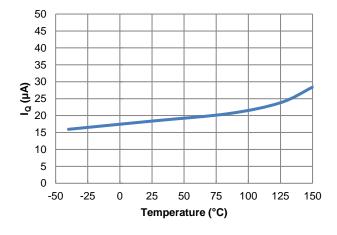


Figure 13. IQ vs. Temperature

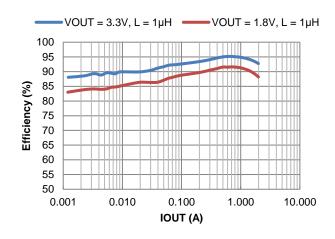


Figure 10. Efficiency vs. Output Current, VIN = 5V

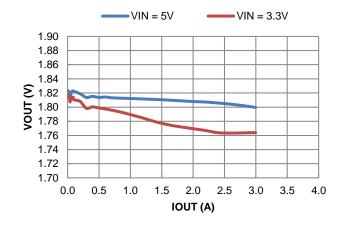


Figure 12. Load Regulation

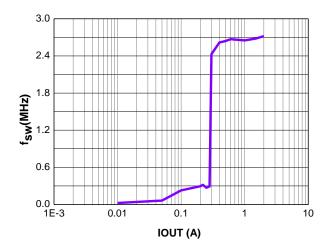


Figure 14. fsw vs. Load



Typical Performance Characteristics (AP61204Q @ TA = +25°C, VIN = 5V, VOUT = 1.8V, BOM = Table 1, PFM, unless otherwise specified.) (continued)

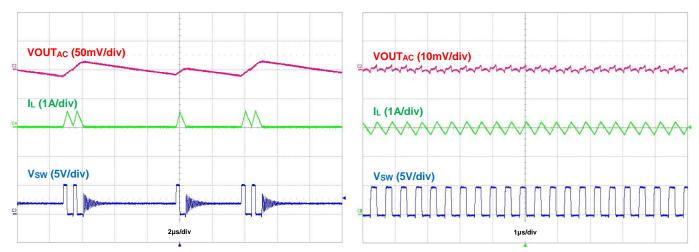


Figure 15. Output-Voltage Ripple, IOUT = 50mA



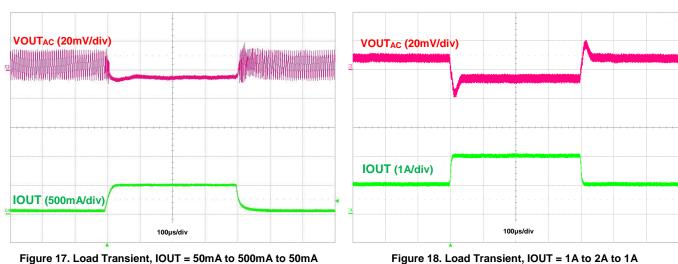


Figure 17. Load Transient, IOUT = 50mA to 500mA to 50mA

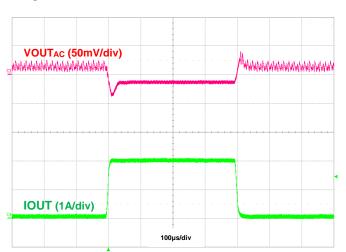


Figure 19. Load Transient, IOUT = 50mA to 2A to 50mA



**Typical Performance Characteristics** (AP61204Q @  $T_A = +25^{\circ}C$ , VIN = 5V, VOUT = 1.8V, BOM = Table 1, PWM, unless otherwise specified.)

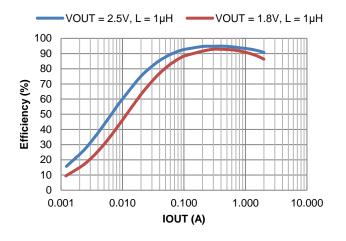


Figure 20. Efficiency vs. Output Current, VIN = 3.3V

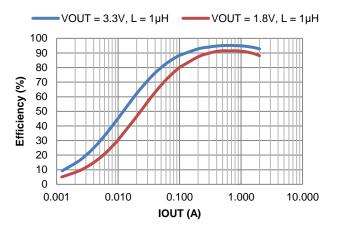


Figure 21. Efficiency vs. Output Current, VIN = 5V

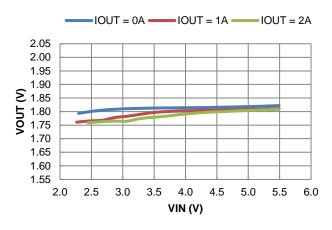


Figure 22. Line Regulation

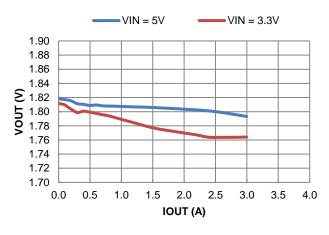


Figure 23. Load Regulation

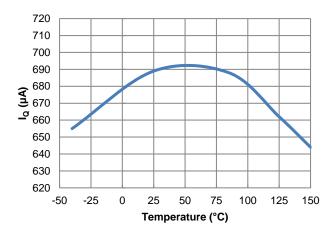


Figure 24. IQ vs. Temperature

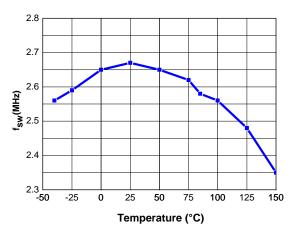
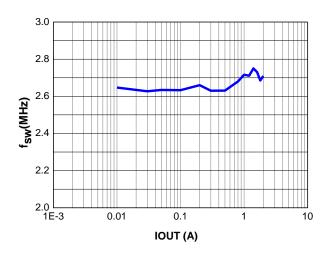


Figure 25. fsw vs. Temperature, IOUT = 0A





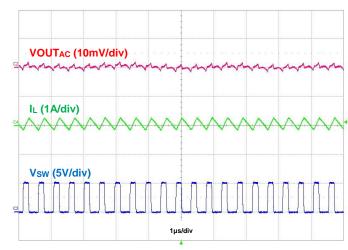
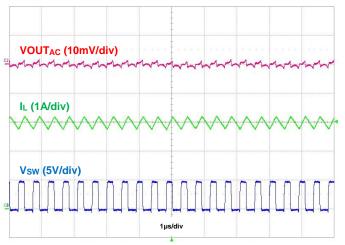


Figure 26. fsw vs. Load

Figure 27. Output-Voltage Ripple, IOUT = 50mA



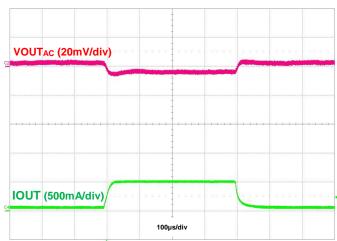
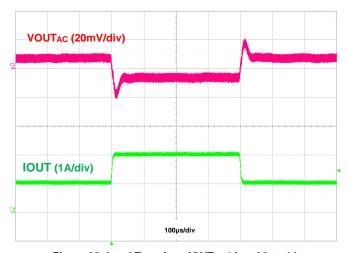


Figure 28. Output-Voltage Ripple, IOUT = 2A

Figure 29. Load Transient, IOUT = 50mA to 500mA to 50mA



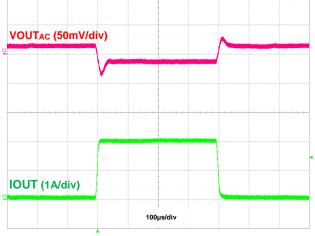


Figure 30. Load Transient, IOUT = 1A to 2A to 1A

Figure 31. Load Transient, IOUT = 50mA to 2A to 50mA



Typical Performance Characteristics (AP61204Q @ T<sub>A</sub> = +25°C, VIN = 5V, VOUT = 1.8V, BOM = Table 1, unless otherwise specified.)

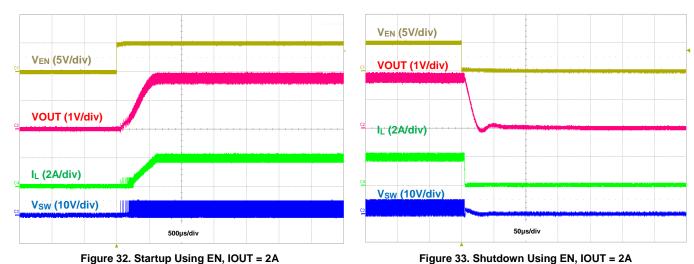


Figure 32. Startup Using EN, IOUT = 2A

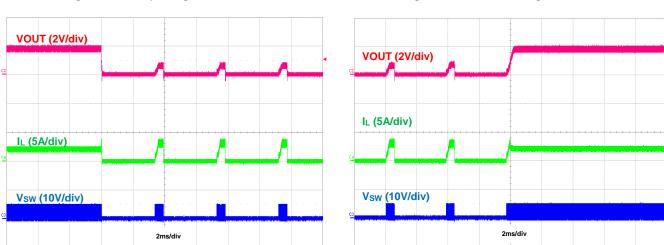


Figure 34. Output Short Protection, IOUT = 2A

Figure 35. Output Short Recovery, IOUT = 2A



**Typical Performance Characteristics** (AP61204Q @ T<sub>A</sub> = +25°C, VIN = 5V, VOUT = 1.8V, BOM = Table 1, unless otherwise specified.) (continued)

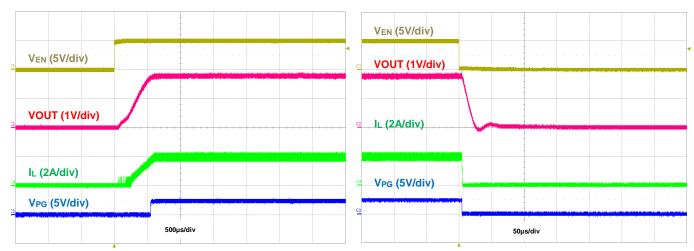


Figure 36. Startup Using EN, IOUT = 2A

Figure 37. Shutdown Using EN, IOUT = 2A

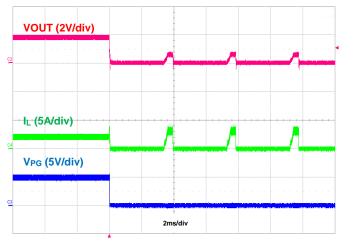


Figure 38. Output Short Protection, IOUT = 2A

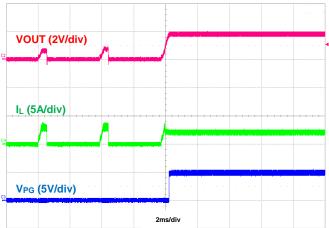


Figure 39. Output Short Recovery, IOUT = 2A



## **Application Information**

### 1 Pulse-Width Modulation (PWM) Operation

The AP61204Q device is an automotive-compliant, 2.4V-to-5.5V input, 2A output, fully integrated synchronous buck converter. Refer to the block diagram in Figure 4. The device employs constant on-time control to provide fast transient response and easy loop stabilization. At the beginning of each cycle, the one-shot pulse turns on the high-side power MOSFET, Q1, for a fixed on-time, ton. This one-shot on-pulse timing is calculated by the converter's input voltage and output voltage to maintain a pseudo-fixed frequency over the input-voltage range. When Q1 is on, the inductor current rises linearly and the device charges the output capacitor. Q1 turns off after the fixed on-time expires, and the low-side power MOSFET, Q2, turns on. Once the output voltage drops below the output regulation, Q2 turns off. The one-shot timer is then reset and Q1 turns on again. The on-time is inversely proportional to the input voltage and directly proportional to the output voltage. It is calculated by the following equation:

$$\mathbf{t_{ON}} = \frac{\mathbf{VOUT}}{\mathbf{VIN} \cdot \mathbf{f_{SW}}}$$
 Eq. 1

Where:

- VIN is the input voltage
- VOUT is the output voltage
- fsw is the switching frequency

The off-time duration is toff and starts after the on-time expires. The off-time expires when the feedback voltage decreases below the reference voltage, which then triggers the on-time duration to start again. The minimum off-time is 70ns typical.

#### 2 Pulse-Frequency Modulation (PFM) Operation

The AP61204Q can be programmed to enter PFM operation at light-load conditions for high efficiency. During light-load conditions, the regulator automatically reduces the switching frequency. As the output current decreases, so too does the inductor current. The inductor current, I<sub>L</sub>, eventually reaches 0A, marking the boundary between Continuous Conduction Mode (CCM) and Discontinuous Condition Mode (DCM). During this time, both Q1 and Q2 are off, and the load current is provided only by the output capacitor. When V<sub>FB</sub> becomes lower than 0.6V, the next cycle begins, and Q1 turns on. Because the AP61204Q can work in PFM during light-load conditions, it can achieve power efficiency of up to 84% at a 5mA load condition.

Likewise, as the output load increases from light load to heavy load, the switching frequency increases to maintain the regulation of the output voltage. The transition point between light and heavy-load conditions can be calculated using the following equation:

$$I_{LOAD} = \left( rac{VIN - VOUT}{2L} 
ight) \cdot t_{ON}$$
 Eq. 2

Where:

. L is the inductor value

The quiescent current of AP61204Q is 19µA typical under a no-load, non-switching condition.



#### 3 Enable

When disabled, the device shutdown supply current is only 0.1µA. When applying a voltage greater than the EN logic-high threshold (typical 0.91V, rising), the AP61204Q enables all functions and the device initiates the soft-start phase. The AP61204Q has a built-in 0.5ms soft-start time to prevent output-voltage overshoot and inrush current. When the EN voltage falls below its logic-low threshold (typical 0.83V, falling), the internal SS voltage discharges to ground and the device operation is disabled.

The device operates in PFM when a logic-high voltage is applied to the EN pin greater than VIN – 200mV. Tying the EN pin to the VIN pin is sufficient to achieve this threshold condition.

The device operates in PWM regardless of output load when a logic-high voltage is applied to the EN pin less than VIN – 200mV. Using an external resistive divider to create a difference in voltage between the VIN and EN pins is sufficient to achieve this threshold condition.

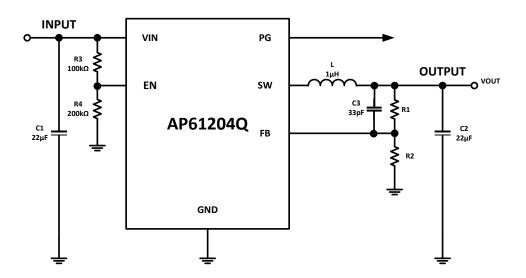


Figure 40. Example Application Circuit for Forced PWM Operation

### 4 Power-Good (PG) Indicator

The PG pin of AP61204Q is an open-drain output that is actively held low during the soft-start period until the output voltage reaches 95% of its target value. When the output voltage is outside of its regulation by  $\pm 10\%$ , PG pulls low until the output returns within 5% of its set value. The PG falling edge transition is delayed by  $40\mu$ s. The PG pin is connected to VIN through an internal  $5M\Omega$  pullup resistor.

### 5 Undervoltage Lockout (UVLO) and Input Overvoltage Protection (OVP)

Undervoltage lockout is implemented to protect the IC from insufficient input voltages. The AP61204Q is disabled if the input voltage falls below 2.2V. In this UVLO event, both the high-side and low-side power MOSFETs turn off and the  $125\Omega$  active discharge is enabled to discharge the output voltage to ground.

Similarly, input overvoltage protection is implemented to protect the IC from excess input voltages. The AP61204Q is disabled if the input voltage rises above 6.3V. In this OVP event, both the high-side and low-side power MOSFETs turn off and the  $125\Omega$  active discharge is enabled to discharge the output voltage to ground.



### 6 Overcurrent Protection (OCP)

The AP61204Q has cycle-by-cycle valley current limit protection by sensing the current through the internal low-side power MOSFET, Q2. While Q2 is on, the internal sensing circuitry monitors its conduction current. The overcurrent limit has a corresponding voltage limit, V<sub>LIMIT</sub>. When the voltage between GND and SW is lower than V<sub>LIMIT</sub> due to excessive current through Q2, the OCP is triggered, and the controller turns off Q2. During this time, both Q1 and Q2 remain off. A new switching cycle begins only when the voltage between GND and SW rises above V<sub>LIMIT</sub>. If Q2 consistently hits the valley current limit for 0.6ms, the buck converter enters hiccup mode and shuts down. After 3.4ms of down time, the buck converter restarts powering up. Hiccup mode reduces the power dissipation in the overcurrent condition.

The AP61204Q also has cycle-by-cycle peak current limit protection by sensing the current through the internal high-side power MOSFET, Q1, through a similar mechanism as the cycle-by-cycle valley current limit protection.

Because the R<sub>DS(ON)</sub> values of the power MOSFETs increase with temperature, V<sub>LIMIT</sub> has a temperature coefficient of 0.4%/°C to compensate for the temperature dependency of R<sub>DS(ON)</sub>.

### 7 Thermal Shutdown (TSD)

If the junction temperature of the device reaches the thermal shutdown limit of +160°C, the AP61204Q shuts down both its high-side and low-side power MOSFETs. When the junction temperature reduces to the required level (+130°C typical), the device initiates a normal power-up cycle with soft-start.

### 8 Power Derating Characteristics

To prevent the regulator from exceeding the maximum recommended operating junction temperature, some thermal analysis is required. The regulator's temperature rise is given by:

$$T_{RISE} = PD \cdot (\theta_{IA})$$
 Eq. 3

Where:

- PD is the power dissipated by the regulator
- θ<sub>JA</sub> is the thermal resistance from the junction of the die to the ambient temperature

The junction temperature, T<sub>J</sub>, is given by:

$$T_{I} = T_{A} + T_{RISE}$$
 Eq. 4

Where:

T<sub>A</sub> is the ambient temperature of the environment

For the SOT563 package, the  $\theta_{JA}$  is 141°C/W. The actual junction temperature should not exceed the maximum recommended operating junction temperature of +150°C when considering the thermal design.



## 9 Setting the Output Voltage

The AP61204Q has adjustable output voltages, starting from 0.6V, using an external resistive divider. The resistor values of the feedback network are selected based on a design trade-off between efficiency and output-voltage accuracy. There is less current consumption in the feedback network for high resistor values, which improves efficiency at light loads. However, values too high cause the device to be more susceptible to noise affecting its output-voltage accuracy. R2 can be determined by the following equation:

$$R2 = \frac{0.6 \cdot R1}{VOUT - 0.6V}$$
 Eq. 5

Table 1 shows a list of recommended component selections for common AP61204Q output voltages referencing Figure 1.

AP61204Q Output Voltage (V) R1 (kΩ) R2 (kΩ) C1 (µF) C2 (µF) C3 (pF) L (µH) 1.0 200.0 301.0 1.0 22 22 1.2 200.0 200.0 1.0 22 22 33 1.5 133.0 1.0 200.0 22 22 33 1.8 200.0 100.0 1.0 22 22 33 2.5 200.0 63.2 1.0 22 22 33 3.3 200.0 44.2 1.0 22 22 33

**Table 1. Recommended Component Selections** 

#### 10 Inductor

Calculating the inductor value is a critical factor in designing a buck converter. For most designs, the following equation can be used to calculate the inductor value:

$$L = \frac{VOUT \cdot (VIN - VOUT)}{VIN \cdot \Delta I_L \cdot f_{SW}}$$
 Eq. 6

Where:

- ΔI<sub>L</sub> is the inductor current ripple
- fsw is the buck converter switching frequency

For AP61204Q, choose ∆I<sub>L</sub> to be 30% to 50% of the maximum load current of 2A.

The inductor peak current is calculated by:

$$I_{L_{PEAK}} = I_{LOAD} + \frac{\Delta I_{L}}{2}$$
 Eq. 7

Peak current determines the required saturation current rating, which influences the size of the inductor. Saturating the inductor decreases the converter efficiency while increasing the temperatures of the inductor and the internal power MOSFETs. Therefore, choosing an inductor with the appropriate saturation current rating is important. For most applications, it is recommended to select an inductor of approximately  $0.47\mu H$  to  $2.2\mu H$  with a DC current rating of at least 35% higher than the maximum load current. For highest efficiency, the inductor's DC resistance should be less than  $30m\Omega$ . Use a larger inductance for improved efficiency under light-load conditions.



## 11 Input Capacitor

The input capacitor reduces both the surge current drawn from the input supply as well as the switching noise from the device. The input capacitor must sustain the ripple current produced during the on-time of Q1. It must have a low ESR to minimize power dissipation due to the RMS input current.

The RMS current rating of the input capacitor is a critical parameter and must be higher than the RMS input current. As a rule of thumb, select an input capacitor with a RMS current rating greater than half of the maximum load current.

Due to large di/dt through the input capacitor, electrolytic or ceramic capacitors with low ESR should be used. If using a tantalum capacitor, it must be surge protected or else capacitor failure could occur. Using a ceramic capacitor of 10µF or greater is sufficient for most applications.

#### 12 Output Capacitor

The output capacitor keeps the output-voltage ripple small, ensures feedback loop stability, and reduces both the overshoots and undershoots of the output voltage during load transients. During the first few microseconds of an increasing load transient, the converter recognizes the change from steady-state and sets the off-time to minimum to supply more current to the load. However, the inductor limits the change to increasing current depending on its inductance. Therefore, the output capacitor supplies the difference in current to the load during this time. Likewise, during the first few microseconds of a decreasing load transient, the converter recognizes the change from steady-state and increases the off-time to reduce the current supplied to the load. However, the inductor limits the change in decreasing current as well. Therefore, the output capacitor absorbs the excess current from the inductor during this time.

The effective output capacitance, COUT, requirements can be calculated from the equations below.

The ESR of the output capacitor dominates the output-voltage ripple. The amount of ripple can be calculated by:

$$VOUT_{Ripple} = \Delta I_L \cdot \left(ESR + \frac{1}{8 \cdot f_{SW} \cdot COUT}\right)$$
 Eq. 8

Output capacitors with large capacitance and low ESR are the best option. For most applications, a total capacitance of 22µF using ceramic capacitors is sufficient. To meet the load transient requirements, the calculated COUT should satisfy the following inequality:

$$COUT > max \left( \frac{L \cdot I_{Trans}^2}{\Delta V_{Overshoot} \cdot VOUT}, \frac{L \cdot I_{Trans}^2}{\Delta V_{Undershoot} \cdot (VIN - VOUT)} \right)$$
 Eq. 9

#### Where:

- I<sub>Trans</sub> is the load transient
- ΔVovershoot is the maximum output overshoot voltage
- ΔV<sub>Undershoot</sub> is the maximum output undershoot voltage



## Layout

## **PCB Layout**

- 1. The AP61204Q works at 2A load current so heat dissipation is a major concern in the layout of the PCB. 2oz copper for both the top and bottom layers is recommended.
- 2. Place the input capacitors as closely across VIN and GND as possible.
- 3. Place the inductor as close to SW as possible.
- 4. Place the output capacitors as close to GND as possible.
- 5. Place the feedback components as close to FB as possible.
- If using four or more layers, use at least the 2<sup>nd</sup> and 3<sup>rd</sup> layers as GND to maximize thermal performance.
- 7. Add as many vias as possible around both the GND pin and under the GND plane for heat dissipation to all the GND layers.
- 8. Add as many vias as possible around both the VIN pin and under the VIN plane for heat dissipation to all the VIN layers.
- 9. See Figure 41 for more details.

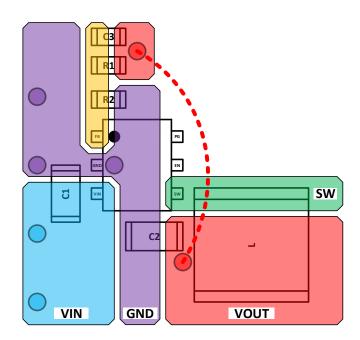
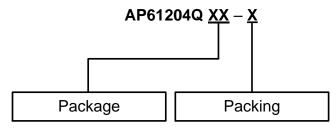


Figure 41. Recommended AP61204Q PCB Layout



# **Ordering Information**



Z6: SOT563

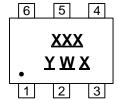
7: Tape & Reel

Part Number	Pookage	Package Code	Packing		
Fait Number	Package	Fackage Code	Qty.	Carrier	
AP61204QZ6-7	SOT563	Z6	3,000	7" Tape and Reel	

# **Marking Information**

### **SOT563**

# (Top View)



 $\underline{XXX}$ : Identification Code  $\underline{Y}$ : Year 0 to 9 (ex: 4 = 2024) W: Week: A to Z: week 1 to 26;

a to z: week 27 to 52; z represents

week 52 and 53 X: Internal Code

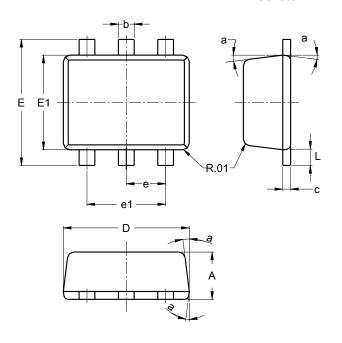
Part Number	Package	Identification Code	
AP61204QZ6-7	SOT563	GSQ	



# **Package Outline Dimensions**

Please see http://www.diodes.com/package-outlines.html for the latest version.

### **SOT563**

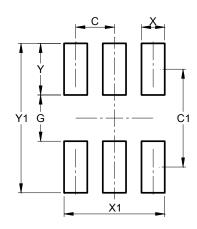


SOT563					
Dim Min Max Ty					
Α	0.55	0.60			
b	0.15 0.30 0.20		0.20		
С	0.10	0.18	0.11		
D	1.50	1.70	1.60		
Е	1.55	1.70	1.60		
E1	1.10	1.25	1.20		
е			0.50		
e1	0.90	1.10	1.00		
L	0.10	0.30	0.20		
а	8°	9°	7°		
All Dimensions in mm					

# **Suggested Pad Layout**

Please see http://www.diodes.com/package-outlines.html for the latest version.

### **SOT563**



Dimensions	Value (in mm)
С	0.500
C1	1.270
G	0.600
Х	0.300
X1	1.300
Y	0.670
Y1	1.940

## **Mechanical Data**

- Moisture Sensitivity: Level 1 per J-STD-020
- Terminals: Finish Matte Tin Plated Leads, Solderable per MIL-STD-202, Method 208 (3)
- Weight: 0.003 grams (Approximate)



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